

Computational Fluid Dynamics: Principles and Applications

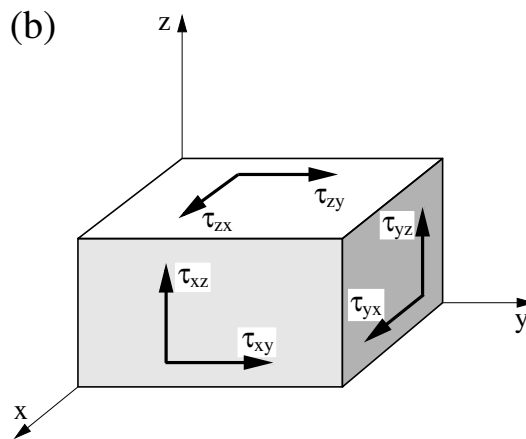
Jiri Blazek, <http://www.cfd-ca.de>

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The following corrections apply to the 3rd edition of the book published in March 2015 by Elsevier Ltd. (ISBN: 978-0-08-099995-1).

Section 2.3: Viscous Stresses

Figure 2.3b on page 15 (stress components got interchanged):



Section 3.1.5: Central and Upwind Schemes

Text on page 42, initial paragraph:

... In this context, it is convenient to differentiate between the discretization of the convective and the viscous fluxes (\vec{F}_c and \vec{F}_v in Eq. (2.19), respectively). ...

Chapter 4: Structured Finite-Volume Schemes

Equation (4.64) on page 96:

$$M_R^- = \begin{cases} 0 & \text{if } M_R \geq +1 \\ -\frac{1}{4}(M_R - 1)^2 & \text{if } |M_R| < 1 \\ M_R & \text{if } M_R \leq -1. \end{cases}$$

Chapter 5: Unstructured Finite-Volume Schemes

Equation (5.9) on page 128:

$$\vec{r}_c = \frac{\Omega_{123} \vec{r}_{c,123} + \Omega_{134} \vec{r}_{c,134}}{\Omega_{123} + \Omega_{134}}.$$

Equation (5.23) and text following on page 135:

$$\vec{n}_{01} \Delta S_{01} = \vec{n}_L \Delta S_L + \vec{n}_R \Delta S_R,$$

and the total face area is given by: $\Delta S_{01} = \|\vec{n}_L \Delta S_L + \vec{n}_R \Delta S_R\|_2$.

Equation (5.62) on page 153:

$$\begin{aligned} \alpha_{ij,1} &= \frac{\Delta x_{ij}}{r_{11}^2} \\ \alpha_{ij,2} &= \frac{1}{r_{22}^2} \left(\Delta y_{ij} - \frac{r_{12}}{r_{11}} \Delta x_{ij} \right) \\ \alpha_{ij,3} &= \frac{1}{r_{33}^2} \left(\Delta z_{ij} - \frac{r_{23}}{r_{22}} \Delta y_{ij} + \beta \Delta x_{ij} \right), \end{aligned}$$

Equation (5.74) on page 162:

$$\left(\frac{\partial U}{\partial \ell} \right)_{IJ} \approx \frac{U_J - U_I}{\ell_{IJ}},$$

Chapter 6: Temporal Discretization

Reference [20] related to Eq. (6.22) on page 176:

Instead, the original reference is: Frink, N.T.; Parikh, P.; Pirzadeh, S.: *A Fast Upwind Solver for the Euler Equations on Three-Dimensional Unstructured Meshes*. AIAA Paper 91-0102, 1991.

Equations (6.76), (6.77) and the related text on page 199:

$$\vec{R}_I^{(p+1)} \approx \vec{R}_I^{(p)} + \bar{J}_I \Delta \vec{W}^{(p)}$$

with $\Delta \vec{W}^{(p)} = \vec{W}^{(p+1)} - \vec{W}^{(p)}$ and $\bar{J} = \partial \vec{R} / \partial \vec{W}$ being the Jacobian matrix. Inserted into Eq. (6.75) while formulated as an iterative procedure, we obtain for the solution at stage k the expression

$$\left[\frac{(\Omega \bar{M})_I}{\Delta t} + a_{kk} \bar{J}_I \right] \Delta \vec{W}^{(p)} = \frac{(\Omega \bar{M})_I}{\Delta t} (\vec{W}_I^n - \vec{W}_I^{(p)}) - \sum_{l=1}^{k-1} a_{kl} \vec{R}_I^{(l)} - a_{kk} \vec{R}_I^{(p)}.$$

This is formally equivalent to Eq. (6.28) and can be solved by any of the implicit methods from the previous subsections. Upon convergence, the solution $\vec{W}^{(p+1)}$ of Eq. (6.77) approximates the intermediate solution at stage k from Eq. (6.75).

Equation (6.85) on page 204:

$$\begin{aligned} \vec{W}_I^{(k)} &= \vec{W}_I^{(0)} - \frac{\alpha_k \Delta t_I^*}{\Omega_I^{n+1}} \left[\bar{I} + \frac{3}{2 \Delta t} \alpha_k \Delta t_I^* \bar{M}^{n+1} \right]^{-1} \\ &\quad \cdot \left[\vec{R}_I(\vec{W}^{(k-1)}) + \frac{3}{2 \Delta t} (\Omega \bar{M})_I^{n+1} \vec{W}_I^{(k-1)} - \vec{Q}_I^* \right]. \end{aligned}$$

Chapter 7: Turbulence Modeling

Equation (7.4) on page 216:

$$\Omega_{ij} = \frac{1}{2} \left(\frac{\partial v_j}{\partial x_i} - \frac{\partial v_i}{\partial x_j} \right).$$

Equation (7.38) on page 226 and the text below it:

$$\begin{aligned} \tilde{S} &= S + \frac{\tilde{\nu}}{\kappa^2 d^2} f_{v2}, \\ f_{v1} &= \frac{\chi^3}{\chi^3 + C_{v1}^3}, \quad f_{v2} = 1 - \frac{\chi}{1 + \chi f_{v1}}, \\ \chi &= \frac{\tilde{\nu}}{\nu_L}, \end{aligned}$$

where S stands for the magnitude of the mean rotation rate, that is,

$$S = \sqrt{2 \Omega_{ij} \Omega_{ij}},$$

and where Ω_{ij} is given by Eq. (7.4). In order to avoid numerical difficulties, the term \tilde{S} must never become zero or negative. One possibility is simple limiting like $\tilde{S} = \max(\tilde{S}, 0.3 S)$. More elaborate approaches were suggested in Ref. [49].

Equation (7.39) on page 226:

$$\begin{aligned} f_w &= g \left(\frac{1 + C_{w3}^6}{g^6 + C_{w3}^6} \right)^{1/6}, \\ g &= r + C_{w2}(r^6 - r), \quad r = \min \left[\frac{\tilde{\nu}}{\tilde{S} \kappa^2 d^2}, 10 \right]. \end{aligned}$$

Equation (7.41) on page 227:

$$\begin{aligned} C_{b1} &= 0.1355, \quad C_{b2} = 0.622, \\ C_{v1} &= 7.1, \quad \sigma = 2/3, \quad \kappa = 0.41, \\ C_{w1} &= C_{b1}/\kappa^2 + (1 + C_{b2})/\sigma, \quad C_{w2} = 0.3, \quad C_{w3} = 2, \\ C_{t1} &= 1, \quad C_{t2} = 2, \quad C_{t3} = 1.2, \quad C_{t4} = 0.5. \end{aligned}$$

Text above Equation (7.42) on page 227:

As pointed out in Ref. [47], it is convenient to substitute the diffusion term in Eq. (7.36), that is,

$$\frac{1}{\sigma} \left\{ \frac{\partial}{\partial x_j} \left[(\nu_L + \tilde{\nu}) \frac{\partial \tilde{\nu}}{\partial x_j} \right] + C_{b2} \frac{\partial \tilde{\nu}}{\partial x_j} \frac{\partial \tilde{\nu}}{\partial x_j} \right\}$$

by the following expression ...

Text to **Initial and boundary conditions** on page 228:

The initial value of \tilde{v} is usually taken as $\tilde{v} = 0.1 v_L$. The same value is also specified at inflow or far-field boundaries. However, in cases where the transition term f_{i1} (and then mostly also f_{i2}) is omitted, that is, for fully turbulent flows, \tilde{v} should be set to 3–5 times the value of v_L at the inlet or far-field. At outflow boundaries, \tilde{v} is simply extrapolated from the interior of the computational domain. At solid walls, it is appropriate to set $\tilde{v} = 0$ and hence $\mu_T = 0$.

References on page 246:

[49] Allmaras, S.R.; Johnson, F.T.; Spalart, P.R.: *Modifications and Clarifications for the Implementation of the Spalart-Allmaras Turbulence Model*. ICCFD7-1902, 7th Int. Conf. on Comput. Fluid Dynamics, 2012.

Chapter 8: Boundary Conditions

Equation (8.7) on page 257:

$$(\vec{F}_{c,w} \Delta S)_{i,2} = \begin{bmatrix} 0 \\ (n_x)_{i-1,2} (p_w)_{i-1/4} \\ (n_y)_{i-1,2} (p_w)_{i-1/4} \\ (n_z)_{i-1,2} (p_w)_{i-1/4} \\ 0 \end{bmatrix} \frac{\Delta S_{i-1,2}}{2} + \begin{bmatrix} 0 \\ (n_x)_{i,2} (p_w)_{i+1/4} \\ (n_y)_{i,2} (p_w)_{i+1/4} \\ (n_z)_{i,2} (p_w)_{i+1/4} \\ 0 \end{bmatrix} \frac{\Delta S_{i,2}}{2}.$$

Equation (8.8) and related text on page 258:

The pressures $(p_w)_{i-1/4}$ and $(p_w)_{i+1/4}$ in Eq. (8.7) can be obtained by linear interpolation, for example,

$$(p_w)_{i+1/4} = \frac{1}{4}(3p_{i,2} + p_{i+1,2}).$$

Chapter 9: Acceleration Techniques

Point 5 of the solution steps described on page 311:

5. Multiply the residual by $\alpha_k \Delta t / \Omega$.

Equation (9.59) on page 313 (last term in the first column):

$$\bar{P} = \begin{bmatrix} \rho_p & 0 & 0 & 0 & \rho_T \\ \rho_p u & \rho & 0 & 0 & \rho_T u \\ \rho_p v & 0 & \rho & 0 & \rho_T v \\ \rho_p w & 0 & 0 & \rho & \rho_T w \\ \rho_p H + \rho h_p - 1 & \rho u & \rho v & \rho w & \rho_T H + \rho h_T \end{bmatrix}.$$

Text on page 318:

... the condition number Eq. (9.40) is reduced (the condition number is $C_N \approx 1.62$) and the ...

A.11 TRANSFORMATION FROM CONSERVATIVE TO CHARACTERISTIC VARIABLES

Matrix of the left eigenvectors Eq. (A.86) on Page 435 (term in the 4th column on the 2nd row):

$$\bar{T}^{-1} = \begin{bmatrix} n_x a_5 - (n_z v - n_y w) \rho^{-1} & n_x a_1 u c^{-2} & n_x a_1 v c^{-2} + n_z \rho^{-1} \\ n_y a_5 - (n_x w - n_z u) \rho^{-1} & n_y a_1 u c^{-2} - n_z \rho^{-1} & n_y a_1 v c^{-2} \\ n_z a_5 - (n_y u - n_x v) \rho^{-1} & n_z a_1 u c^{-2} + n_y \rho^{-1} & n_z a_1 v c^{-2} - n_x \rho^{-1} \\ a_2(\varphi - cV) & -a_2(a_1 u - n_x c) & -a_2(a_1 v - n_y c) \\ a_2(\varphi + cV) & -a_2(a_1 u + n_x c) & -a_2(a_1 v + n_y c) \\ n_x a_1 w c^{-2} - n_y \rho^{-1} & -n_x a_1 c^{-2} \\ n_y a_1 w c^{-2} + n_x \rho^{-1} & -n_y a_1 c^{-2} \\ n_z a_1 w c^{-2} & -n_z a_1 c^{-2} \\ -a_2(a_1 w - n_z c) & a_1 a_2 \\ -a_2(a_1 w + n_z c) & a_1 a_2 \end{bmatrix}.$$